

Antenna Array Design Using Microwave Photonics Technology

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Microwave Photonics – Impact and Applications

Microwave photonics: Here: Coherent optical generation of radiation (MWP) (temporally sinusoidal electric field) with frequencies from several GHz up to the THz-range

$2 \text{ GHz} \leq f \leq 60 \text{ GHz}$: Electronic generation of spectrally pure microwave signals, inexpensive distribution to many receivers via optical fibres, local demodulation, inexpensive electronic amplification
 $(15 \text{ cm} \geq \lambda \geq 5 \text{ mm})$

Applications: Terrestrial communication (mobile phones, office, "last mile"), radar, inter-satellite communication, sensors

$60 \text{ GHz} \leq f \leq 100 \text{ GHz}$: Electronic signal generation more difficult, electronic amplifiers not yet standard products
 $(5 \text{ mm} \geq \lambda \geq 3 \text{ mm})$

Applications: Radar, inter-satellite communication, sensors (distance)

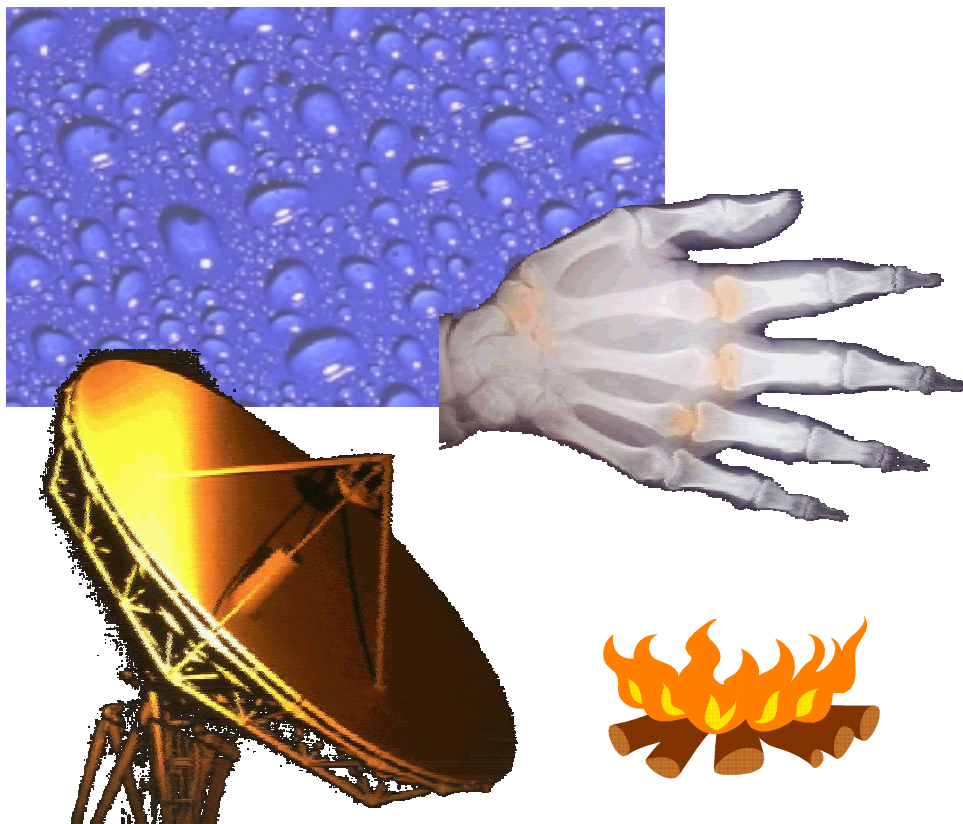
$100 \text{ GHz} \leq f \leq 10 \text{ THz}$: Electronic signal generation uneconomical or impossible, no electronic amplifiers available
 $(3 \text{ mm} \geq \lambda \geq 30 \text{ }\mu\text{m})$

Applications: Radar, imaging, sensors, medical diagnostics



A look into the future: Terahertz Photonics – What are T-rays?

Quality control, medical diagnostics, gas spectroscopy

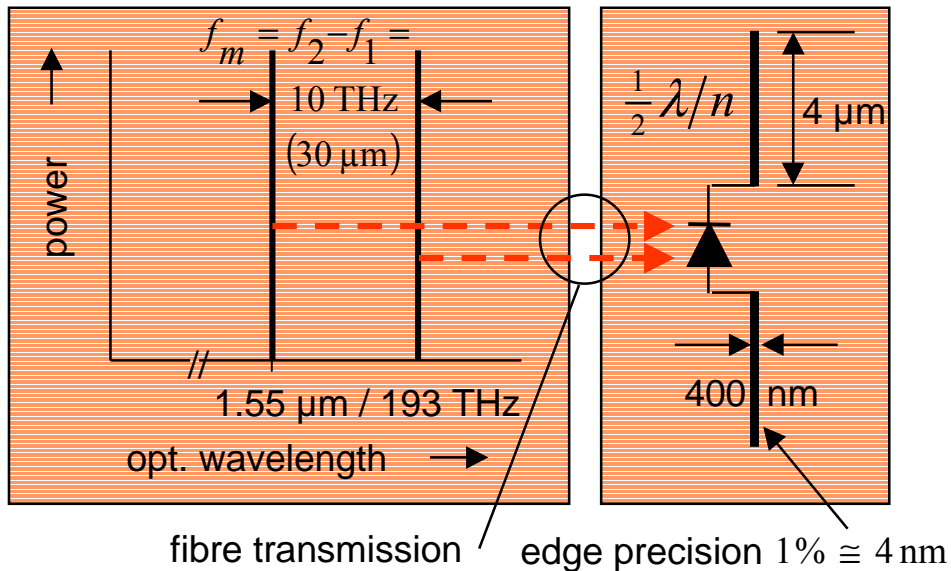


- **Humidity (absorption lines 0.6 ... 2 THz, CLEO '98 CTuB5, Opt. Lett. 14 (1989) 1128): production of food**
- **Dermatology: Structure of burned skin without biopsy**
- **Tomography (Opt. Lett. 22 (1997) 904)**
- **T-rays replace Roentgen rays (X-rays):
Imaging of "invisible" objects
Inspection of pallets
Airport safety measures, drug detection**
- **Analysis of flames and gases (toxicity, Fourier spectrum)**
- **Quality control: Holes in plastic parts, plastics for car production**
- **Radar applications (measurement of reflection)**



Terahertz Photonics – Generation of Coherent T-Rays

Mixing of two optical signals by a Schottky photodiode



- 2 optical lines, difference frequency 10 THz
- Schottky diode as photodetector-mixer.
Lateral dimensions in 1- μm range
(Light focus dimension $0.61 \cdot \lambda = 1 \mu\text{m}$)
Junction capacitance $C \approx 3 \text{ fF}$
Series resistance $R \approx 5 \Omega$ (!)
RC corner frequency $f_c \approx 11 \text{ THz}$
- Integrated antenna, λ -dipole for 10 THz.
High edge precision in nm-range necessary
- Receiving antenna with similar structure as detector of T-rays

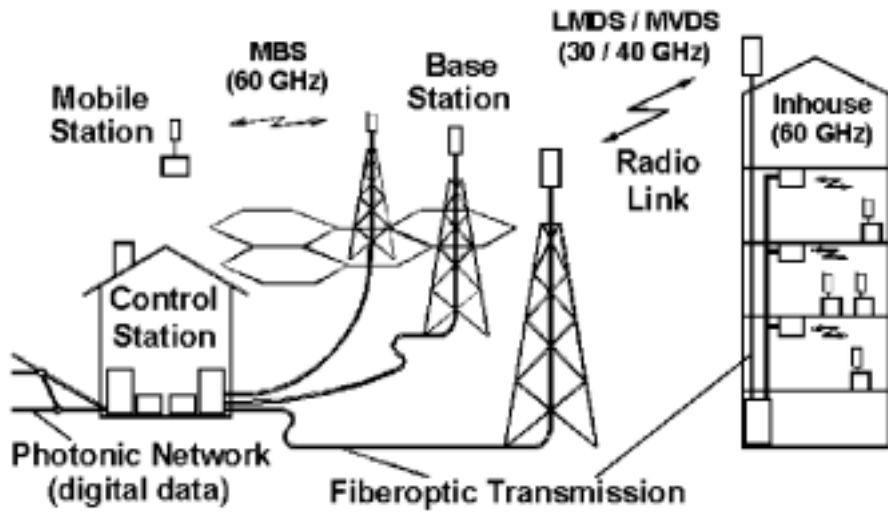
Technological Problems and Challenges

- Electrochem. nano-structuring of Schottky PD: Substrate n-Si; metal (e.g. Pb); junction C ; series R
- Corrosion and passivation, accuracy, edge precision, and transmission line loss (type e.g. coplanar)



Microwave Photonics – What Can Hybrid Techniques Do?

Micro and picocellular networks (HFR, Hybrid Fibre Radio)



Few expensive control stations with frequency-stable microwave generators, numerous inexpensive base stations with opto-electronic converters and MMIC microwave amplifiers.

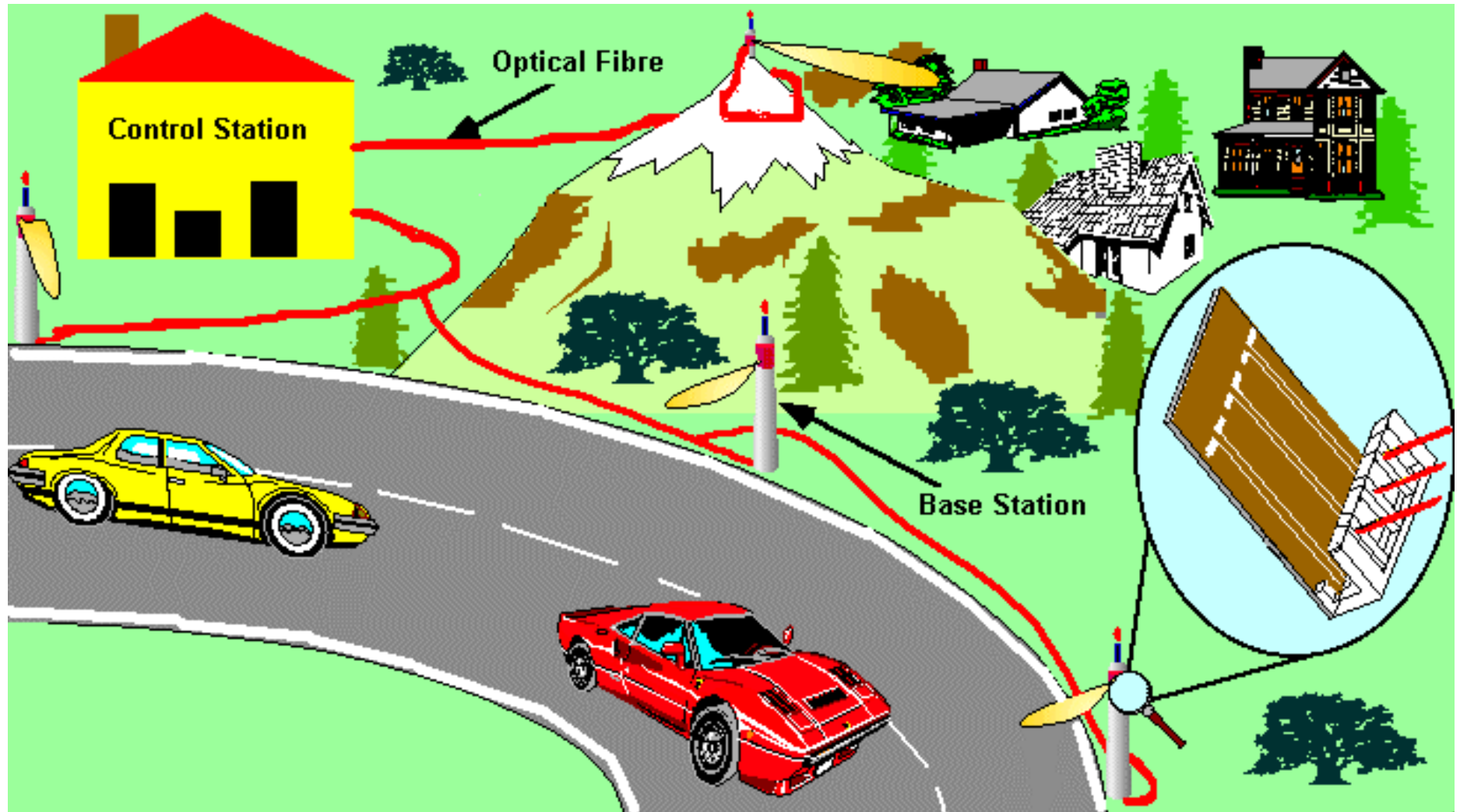
- Local Multipoint & Multipoint Video Distribution System (LMDS & MVDS)
- Mobile Broadband Systems (MBS)
- In-House, shop, and hangar systems
- Telematics, sensors, military and satellite communication

Operation principle:

Data signals modulated on optical carrier, via low-loss fibre transmitted, in base station demodulated und radiated.

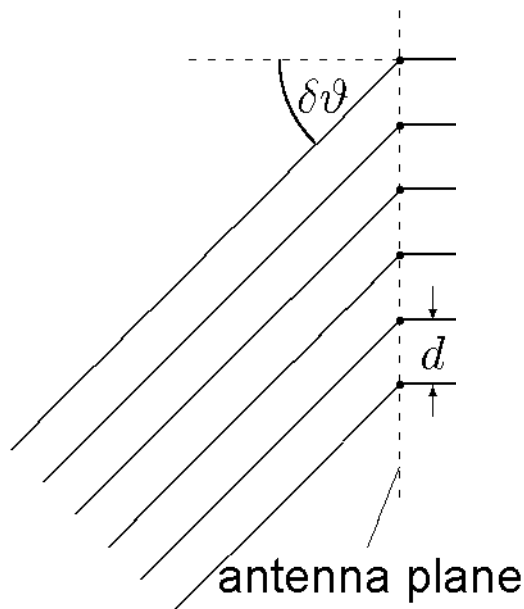


Example of HFR Control and Base Stations



Antenna Array, Beam Squint, and Beamforming Network (1)

Antenna array beam steering and squint



- Problems with RF beamforming network (BFN):
- High losses, high dispersion, interference with microwave transm. lines and fields, bulky, complicated mechanical arrangement

- Antenna array modelled by linear array of point sources (•, `grating` constant d), $\delta\varphi = 0$
- Propagation in 1st diffraction order direction, tilted from normal $\vartheta = 90^\circ$ by $\delta\vartheta$
- Well known diffraction formula $\sin(\delta\vartheta) = \lambda_m / d$
- With arbitrary $\delta\varphi$ at •, 0th order beam direction tilted by:

$$\sin(\delta\vartheta) = \frac{\lambda_m}{d} \frac{\delta\varphi}{2\pi} = \frac{c}{\omega_m} \frac{\delta\varphi}{d}$$

- If subcarrier f_m varies with time t : beam squint $\delta\vartheta(t)$ for $\delta\varphi = \text{const}_t$
- No squint even with wide bandwidth signal, if

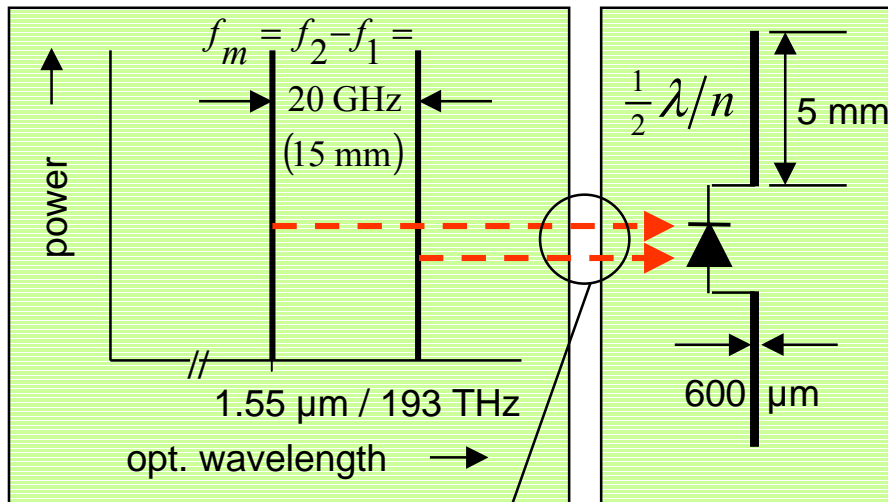
$$\delta\varphi \sim \omega_m$$

for all ω_m !



Antenna Array, Beam Squint, and Beamforming Network (2)

Recipe for RF transmission and optical beamforming network



fibre transmission, length L

Beauties of optical TTD

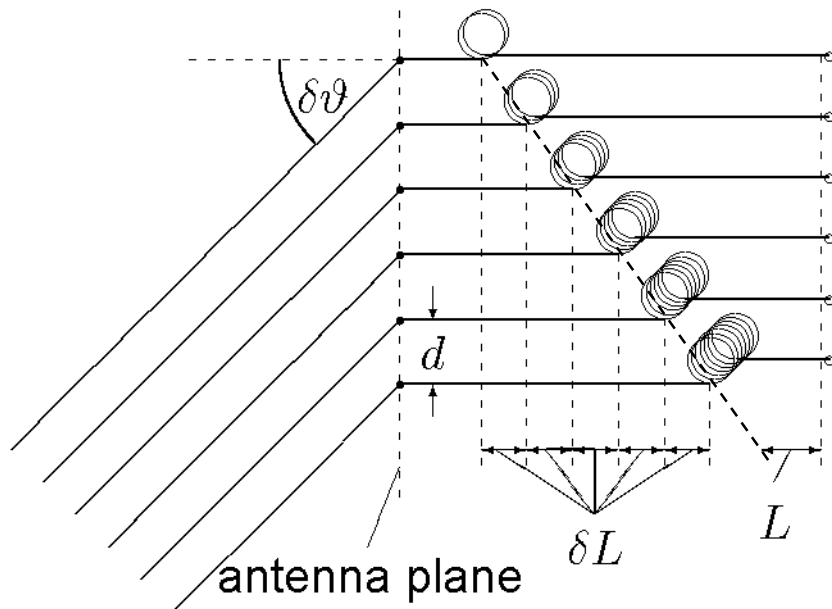
- Low volume, light, inexpensive
- Very low loss, very low dispersion

- 2 optical lines, difference frequency $f_m = 20 \text{ GHz}$
- RF modulation signal transferred to one of the optical lines
- Transmit by optical single-mode fibre
- Detect original RF signal from optical carrier by mixing modulated and unmodulated line
- Mixing by detecting optical power with photodetector (quadratic demodulator, but no sum frequency!)
- Photocurrent contains the IF $f_m = f_2 - f_1$
- Amplify the photocurrent
- Radiate resulting signal by each antenna element
- Adjust the beamforming network by the lengths L of the optical fibres, either mechanically, or optically



Antenna Array, Beam Squint, and Beamforming Network (3)

Avoiding beam squint by TTD



- Microwave photonics makes *optical* feeder network possible, greatly reduces problems of a true time delay (TTD) network:
- Low losses, low dispersion, not bulky, no interference with microw. transm. lines & fields

TTD schematic (True Time Delay Network)

- Linear array modelled by linear array of point sources •, fed at o with identical phases by delay lines of length $L_i = L + i\delta L$ with length increments δL
- RF current phase difference at • expressed by group delay time increment δt_g or, with group velocity v_g , by

$$\delta\phi = \omega_m \delta t_g = \omega_m \frac{\delta L}{v_g}$$

No beam squint

- With arbitrary f_m and δL , 0th order beam direction tilted by

$$\sin(\delta\vartheta) = \frac{\lambda_m}{d} \frac{\delta\phi}{2\pi} = \frac{c}{\omega_m} \frac{\delta\phi}{d} = \frac{c}{v_g} \frac{\delta L}{d}$$



RF Signal Fibre Transmission

Details of RF transmission over dispersive single-mode fibre

Transfer function of opt. transm. fibre, length L_i :

$$\check{h}_i(f) = \exp[-j\beta_i(\omega)L_i]$$

Feeds opt. receivers \rightarrow RF drive of antenna elem.

Prop. const. β , group delay time $t_g/L = 5\mu\text{s}/\text{km}$,
chromatic dispersion $C = 17\text{ ps}/(\text{km nm})$:

$$\beta_i \approx \beta(\omega_0) + (\omega - \omega_0) \frac{t_g}{L_i} - \frac{(\omega - \omega_0)^2}{2} \frac{\lambda_0^2}{2\pi c} C$$

Fibre length incr. @ RF mod. freq. $f_m = 20\text{GHz}$:

$$\delta L_{\max} = \frac{v_g}{c} d = \frac{2}{3} \frac{\lambda_m}{2} = \frac{15}{3} \text{ mm} = 5 \text{ mm}$$

Group delay time increment:

$$\delta t_{g \max} = \frac{\delta L_{\max}}{v_g} = \frac{d}{c} = \frac{\lambda_m}{2c} = \frac{1}{2f_m} = 25 \text{ ps}$$

Chrom. delay time err. for spectr. width $\Delta f = f_m$:

$$\Delta f = 20 \text{ GHz}, \quad \Delta \lambda = \frac{(1.55 \mu\text{m})^2}{c} \Delta f = 0.16 \text{ nm}$$

$$\delta t_{gC} = C \delta L_{\max} \Delta \lambda = 14 \text{ fs} = 0.6 \times 10^{-3} \delta t_{g \max}$$

Summary:

Chromatic dispersion unimportant for OBFN

Fibre output spectrum from transfer function :

$$\check{a}_L(f) = \check{h}(f) [\delta(f - f_1) + \delta(f - f_2)]$$

PD detects opt. power (quadr. demodul. for f_m ,

no optical sum frequency!), RF current $i(t)$:

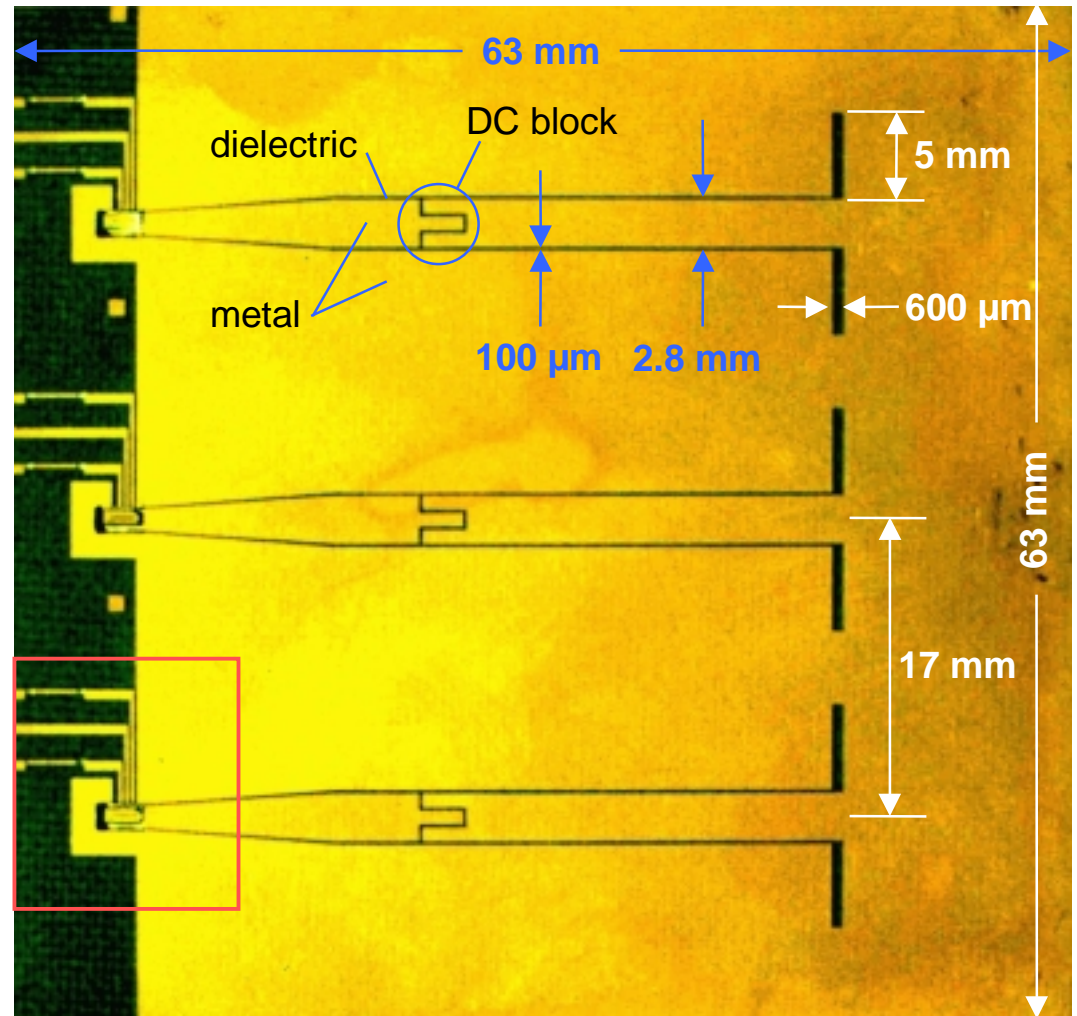
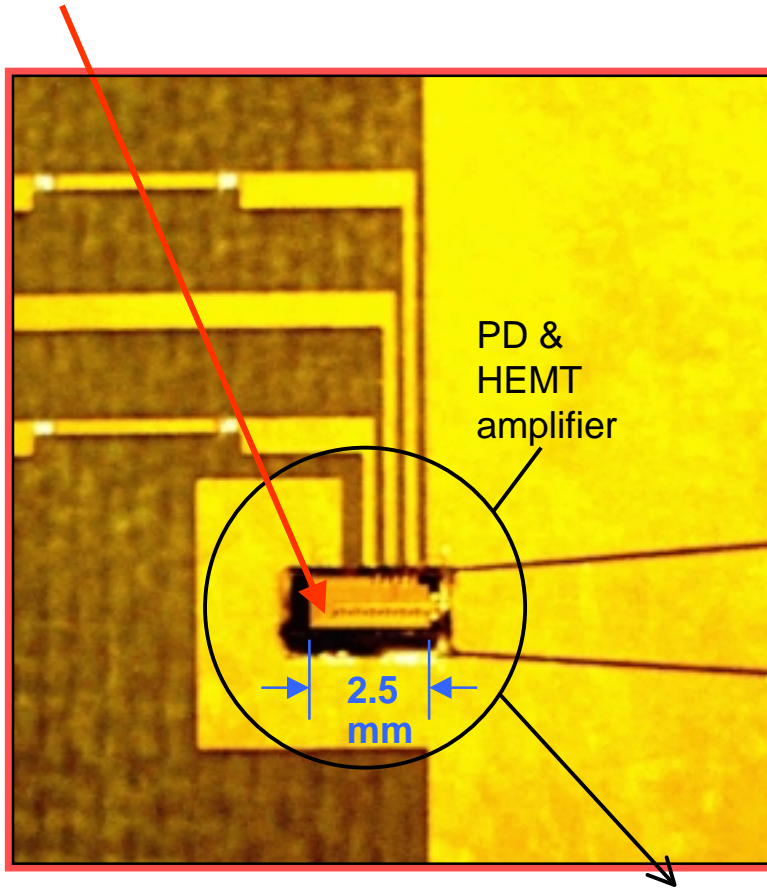
$$i(t) \propto \left\langle \left| F^{-1} \{ \check{a}_L(f) \} \right|^2 \right\rangle \propto \cos(\omega_m t - \omega_m t_g)$$

$\varphi_i \propto \omega_m L_i$

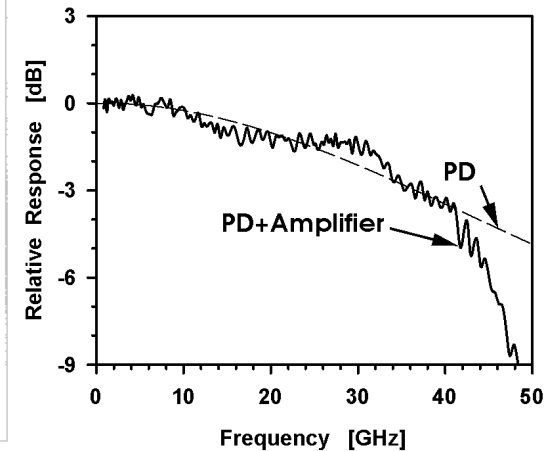
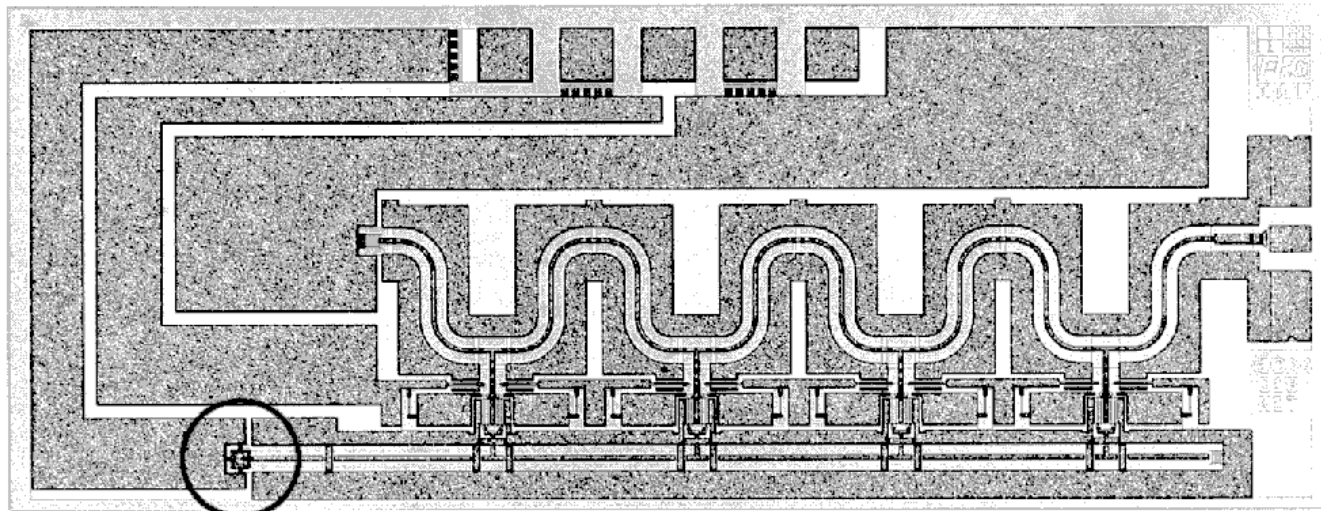


λ -Dipole Antenna with Optical Feeder at 20 GHz

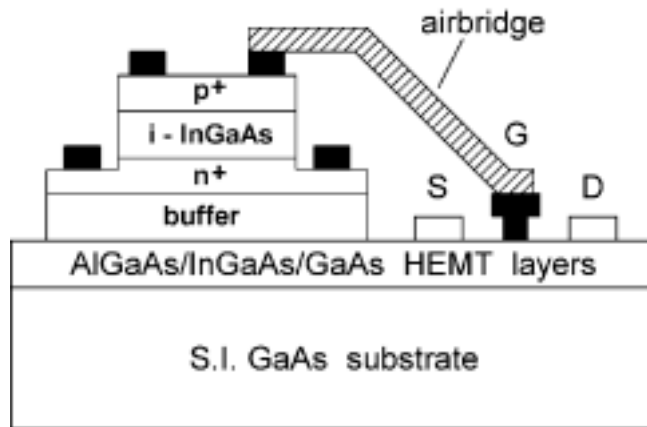
Each of 3 antenna elements separately fed via **single-mode glass fibre**, which illuminates **PD** from top.



HEMT Photoreceiver (IAF, Hurm et al. ECOC 1998)



PIN-PD

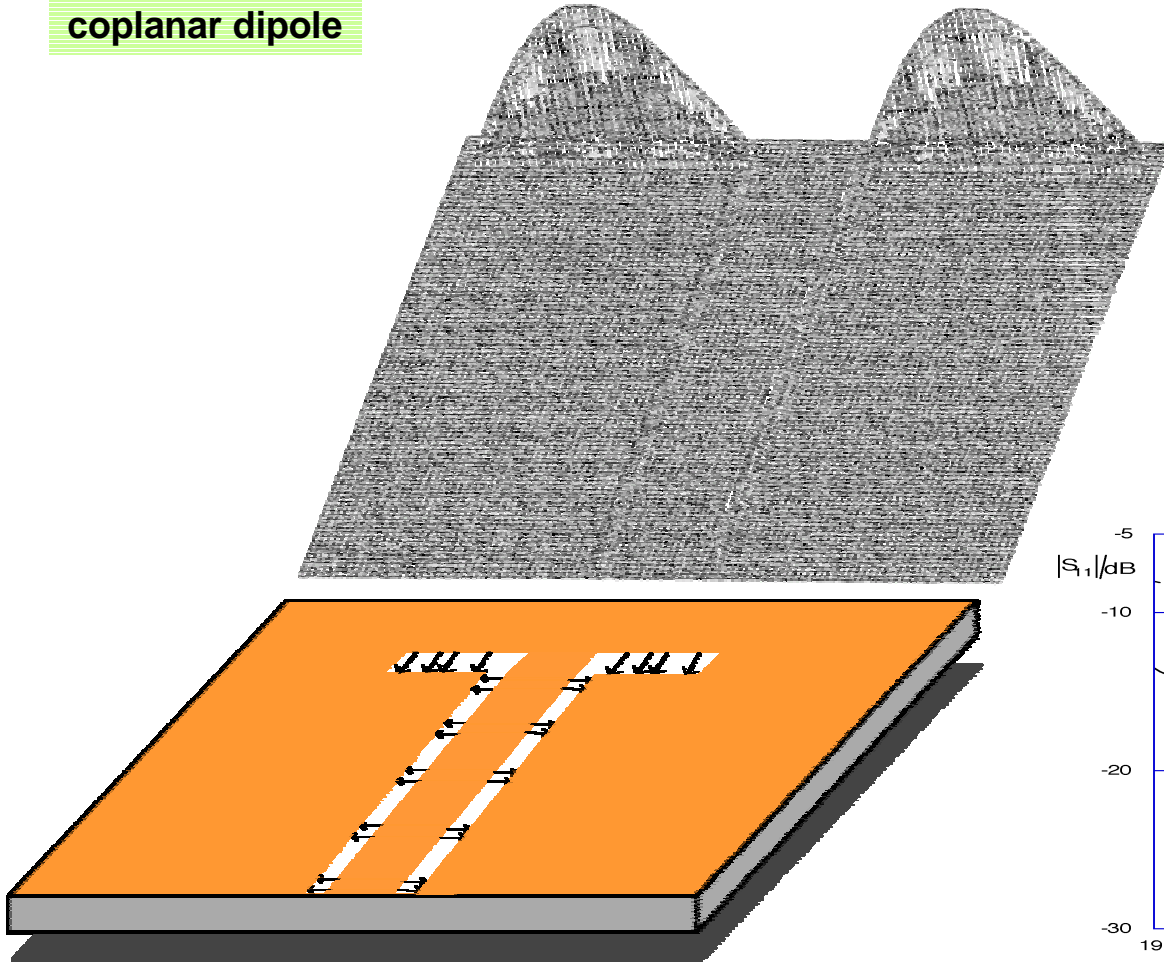


- OEIC on semi-insulating GaAs (2.5 mm × 1 mm)
- PD 10 μmØ, 3-dB bandw. 36.5 GHz @ 25 Ω, RC limited (---)
- Distributed amplifier with 4 HEMT stages
- Cascoded pseudomorphic HEMT
 Gate length 150 nm, InGaAs channel 12 nm
 Transconductance $g_m = 754 \text{ mS / mm}$, current-gain cut-off frequency $f_T = 90 \text{ GHz}$,
 Maximum oscillation frequency $f_{\text{max}} = 150 \text{ GHz}$
 Coplanar 50-Ω output

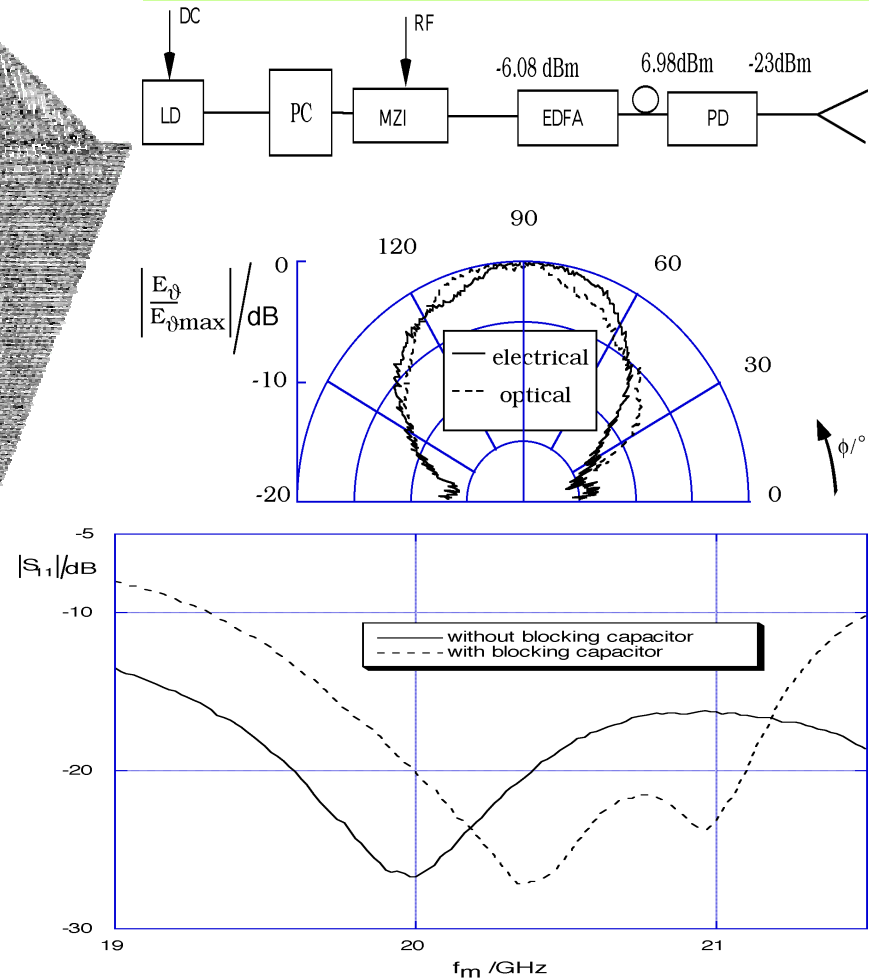


Coplanar λ -dipole at 20 GHz

Electric field at coplanar dipole



Radiation pattern and input impedance



Summary and Outlook

Present state

- Data transmitted to base stations via photonic networks
- Application of MWP (here: at 20 GHz) mainly for *radio communication and sensors*
- Mass market for bridging the “last mile” for connecting subscribers to *broadband communication networks* without road works
- With optical beamforming networks, the radiation patterns don't show “*beam squint*”
- Length reconfiguration of fibre feeders for *spatial beam tracking*

Microwave photonics

- Upgrade of model system from 20 GHz to higher frequencies, e.g., 40 GHz
- Design and test of optical beamforming networks
- Antenna design for semiconductor substrates with refractive indices near $n = 3,6$
- Problems: Radiation efficiency
Amplifier heat removal

Future work

Future Terahertz Photonics

- Design of THz transm. lines with edge precision in the 4-nm region on semicond. substrates; losses
- Design and investigation of photo-sensitive Schottky diodes
- Antenna design

